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## CHANGES IN THE PERMEABILITY, STREAMING POTENTIAL AND RESISTIVITY OF A CLAYSTONE FROM THE NANKAI PRISM UNDER STRESS.

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Abstract. Permeability is the critical factor governing fluid flow in accretionary prisms. Accretionary wedges are highly deformed, so permeability changes in an indurated claystone sample from the Nankai accretionary prism were measured during a triaxial stress experiment by the pulse decay method. Three zones were identified from the loading test. In zone I, the sample has deformed less than 1.3% and its permeability was  $5 \cdot 10^{-20} \text{ m}^2$ . In zone II, the deformation reached 1.5% and the permeability was unstable with time. In zone III, the sample deformation reached 2% and its permeability reached  $3.8 \cdot 10^{-18} \text{ m}^2$ . The permeability strongly decreased (from  $3.2 \cdot 10^{-18} \text{ m}^2$  to  $1.7 \cdot 10^{-19} \text{ m}^2$ ) with increasing effective pressure (from 2.3 to 10.8 MPa) after the sample was well deformed (zone III). The streaming potential was not measurable when the sample had a low permeability (zone I), but clearly occurred when the permeability increased (zone III) : the streaming potential measured was 6 mV when the pore pressure pulse applied was about 1.17 MPa and the permeability  $3.8 \cdot 10^{-18} \text{ m}^2$ . Our experiments suggest that shear deformation under low effective pressure increased the vertical permeability of sediments above the décollement. This increase in permeability may be detected by measuring the streaming potential. Variations of flow rate of expelled fluid in accretionary wedges may be detected by monitoring changes of electrokinetic potential, giving new insights on the state of stress related to the seismic cycles.

### Introduction

Elevated pore fluid pressure has long been recognized to maintain large parts of accretionary prisms near failure conditions [von Huene and Lee, 1982], resulting in complex interactions of strain regimes and fluid circulation. Expelled fluids from accretionary wedges have been shown to be transported from great depth within the prism [Moore and

Vrolijk, 1992]. The use of Darcy's law as governing equation of fluid flow in a prism [Henry and Wang, 1991] is probably reasonable as the high density of interconnected fractures probably approximates a Darcian continuum over large length scales. As expressed by Darcy's law, fluid pressure gradients are the driving force of fluid flow while rock permeability resists fluid flow. Pressure gradients change less than 1 order of magnitude, although permeability changes can be of 6 to 8 orders of magnitude [Moore and Vrolijk, 1992]. The permeability is thus the critical factor governing fluid flow in accretionary wedges. We present results from an experimental study of the changes of permeability associated with the deformation of an indurated claystone sample from the Nankai accretionary wedge. The permeability was measured as a function of the effective pressure for different states of axial strain. Variation of the electrical resistivity was measured during the experiment. We also measured the streaming potential during the measurement of permeability by pore pressure diffusion.

### Sampling and experimental procedure

The two samples studied were obtained from leg 131 (hole 808C) of the Ocean Drilling Program, in the Nankai accretionary wedge. One sample was a tuff (sample 131-808C-54R-1, 68-72cm), collected from about 810 meters below the sea floor (mbsf), and the other was an indurated claystone (sample 131-808C-102R-1, 121-126 cm), from about 1260 mbsf, with porosity of 23% and bulk density of  $2.4 \text{ g/cm}^3$ . Both samples were from below the décollement and thus belong to an undeformed sequence [Taira et al., 1992]. Samples were cut into cylinders : 20 mm in diameter and 40 mm long. They were saturated with distilled water and isolated from the confining pressure by a jacket. We used a press with controlled displacement. Variations of axial pressure, confining pressure and pore pressure were independant. Samples were first subjected to an axial stress and a confining pressure of  $11 \pm 0.1 \text{ MPa}$ , and a pore pressure of  $9 \pm 0.1 \text{ MPa}$ . These values were raised after a period of time sufficient to nearly equilibrate the pore pressure due to diffusion.

Vertical permeability was determined by the pulse decay method [Brace et al., 1968], which follows the decay of a small step change of pore pressure imposed at one end of a sample. When a pressure pulse  $\Delta P_0$  (less than 10% the magnitude of the total pore pressure) is generated, the

differential pressure  $\Delta P(t)$  decays exponentially as a function of time,  $t$  :

$$\Delta P(t) = 2 \Delta P_0 V_2 / (V_1 + V_2) e^{-mt} \quad (1)$$

where  $V_1$  and  $V_2$  are the upstream and downstream reservoir volumes ( $V_1=V_2=50 \cdot 10^{-6} \text{ m}^3$  in our experimental setup, large compared with the sample pore volume which is  $2.9 \cdot 10^{-6} \text{ m}^3$ ),  $t$  is time and  $m$  is a decay time constant. Plotting the decay curve in terms of  $\ln(\Delta P(t))$  versus time  $t$  yields a straight line having a slope  $m$ , and the permeability  $k$ , can be determined by  $k = (m \mu \beta L V_1 V_2) / (A(V_1 + V_2))$  where  $L$  is the length of the sample,  $A$  the cross-sectional area of the sample,  $\mu$  the dynamic viscosity of pore fluid at temperature measurement ( $10^{-3} \text{ Pa.s}$  at  $20^\circ\text{C}$ ), and  $\beta$  is the compressibility of the pore fluid ( $0.42 \cdot 10^{-9} \text{ Pa}^{-1}$ ). The pulse decay method is time-consuming because the diffusion of the pressure pulse across a clay sample can be about 24 hours and we must wait at each step for the total diffusion of the pore pressure inside the sample. Our apparatus was tested by measuring the permeability to water of a sample of Fontainebleau sandstone (France) with a porosity of 4.3% and a permeability to air of  $4 \cdot 10^{-16} \text{ m}^2$ , giving us the opportunity to measure the permeability to water using two different methods. We found  $k=2.2 \cdot 10^{-16} \text{ m}^2$  with the steady state flow method and  $k=1.1 \cdot 10^{-16} \text{ m}^2$  with the pulse decay method, and concluded that our experimental method and the use of (1) yield reliable values of the permeability.

The pulse decay method has been used in triaxial tests on granite [Brace et al., 1968, Bernabé, 1987], and on samples of tuff [Zhang et al., 1993]. But permeability of argillaceous rocks is generally measured using a consolidation test [Taylor and Fisher, 1993]. Because the permeability of clays is supposed to be sensitive to the effective pressure [Brace, 1980], we made measurements of permeability at different states of effective stress.

The resistivity of the samples was measured at 4 kHz with an impedancemeter. The streaming potential is the difference of potential across a sample when a fluid is made to flow through it by a driving pressure  $\Delta P$ . This streaming potential was measured by a voltmeter with an input resistance greater than  $10^{10} \Omega$ .

## Experimental results

### Permeability measurements

The sample of tuff had a permeability of  $3.5 \pm 1.5 \cdot 10^{-20} \text{ m}^2$  (or  $3.5 \cdot 10^{-11} \text{ cm/s}$ ) when subjected to an axial stress and a constant confining pressure of 11 MPa, and a pore pressure of 9.2 MPa. Unfortunately, this sample was crushed because of a power cut and we could not make further measurements.

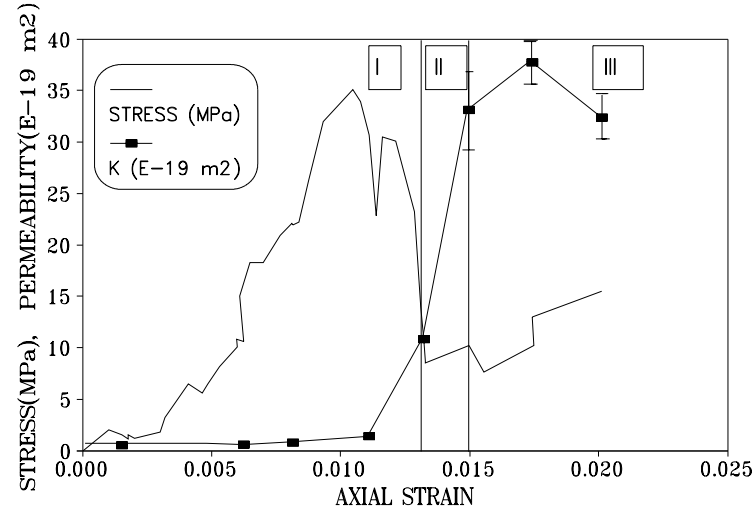


Fig. 1. : Differential stress (continuous line) and permeability as a function of axial strain (square dots). Zone II represents a critical strain where the permeability is unstable. Permeability changes from  $5 \cdot 10^{-20} \text{ m}^2$  to  $3.8 \cdot 10^{-18} \text{ m}^2$  in a narrow range of axial stress.

The second sample was exposed to an increasing deviatoric stress, with a confining pressure of 12 MPa, and a pore pressure of 9.2 MPa. The entire experiment lasted 11 days and the sample was deformed at an average strain rate of  $2.3 \cdot 10^{-8} \text{ s}^{-1}$ . The timing of the measurements was kept as constant as possible. The differential stress (axial stress minus confining pressure) and the permeability as a function of the axial strain are represented in Figure 1. First, the permeability was  $5 \cdot 10^{-20} \text{ m}^2$ , and remained almost constant up to the stress drop (Zone I). This stress drop, from 35 MPa to 10 MPa, occurred during a 49 hours period. Then the permeability increased up to  $1.1$  and  $3.3 \cdot 10^{-18} \text{ m}^2$  (Zone II) and remained high :  $3.2$  to  $3.8 \cdot 10^{-18} \text{ m}^2$  when the sample was further deformed (Zone III). Zone II represents a critical deformation where the permeability was unstable. At the Zone I-II transition, two measures of permeability were made at constant axial strain : it decreased with time from  $2 \cdot 10^{-18} \text{ m}^2$  to  $1.2 \cdot 10^{-18} \text{ m}^2$  as shown in Figure 2. At

the Zone II-III transition, permeability increased with time from  $1.8 \cdot 10^{-18} \text{ m}^2$  to  $3.3 \cdot 10^{-18} \text{ m}^2$ . The time needed for each measure of permeability is shown by horizontal line.

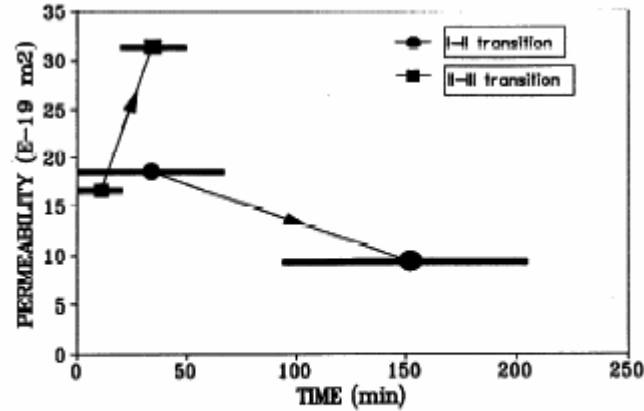


Fig. 2. : Evolution of the permeability with time at the I-II and II-III transitions (Fig.1.). The time needed for a permeability measurement is shown by horizontal line.

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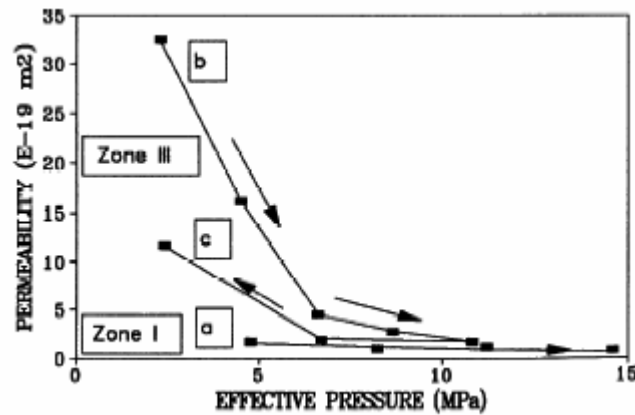


Fig. 3. : Permeability versus the effective pressure. a- in zone I, b- in zone III, by increasing confining pressure; c- in zone III, by increasing pore pressure.

The permeability was then measured as a function of the effective pressure (confining pressure minus pore pressure) between 2 and 15 MPa. In zone I the permeability did not vary with the effective pressure as shown in Figure 3. On the other hand the permeability in zone III (after the last permeability measurement shown in Figure 1) became very

sensitive to the effective pressure : the permeability decreased from  $3.2 \cdot 10^{-18} \text{ m}^2$  ( $P_e=2.3 \text{ MPa}$ ) to  $1.7 \cdot 10^{-19} \text{ m}^2$  ( $P_e=10.8 \text{ MPa}$ ). When the effective pressure was decreased by an increase of pore pressure to  $P_e=2.3 \text{ MPa}$ , the permeability increased but did not recover its initial value ( $3.2 \cdot 10^{-18} \text{ m}^2$ ). At the end of the experiment, no macroscopic shear fracture was observed. For this clay sample, the well-oriented clay flakes deformed by shear stress probably produced interconnected fluid volumes, resulting in an increase of permeability.

### Electrical measurements

The resistivity decreased during the first stage of deformation, then it increased in zone II and III as shown in Figure 4. For this sample, the electrical conductivity was due not only to electrolytic conduction, but also to the surface conductivity. Moreover, the electrical conductivity of the fluid changed through chemical interaction during the 10 days of the experiment from  $1500 \text{ } \Omega \cdot \text{m}$  (initial saturating fluid) to  $90 \text{ } \Omega \cdot \text{m}$  at the end of the experiment (determined from collected water when the sample was taken off the cell), resulting in a complex behavior of the resistivity with the deformation. This behavior is opposite to that observed in sandstones, whose mechanical behavior is brittle with dilatancy, and whose electrical conductivity is only due to the electrolytic conduction [Jouniaux et al., 1992].

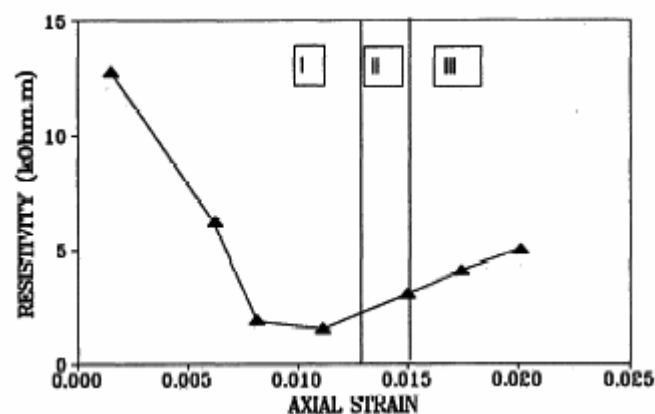


Fig. 4. : Electrical resistivity of the rock versus axial strain. The behavior of the resistivity includes the electrolytic conduction, the surface conductivity, and the chemical interaction.

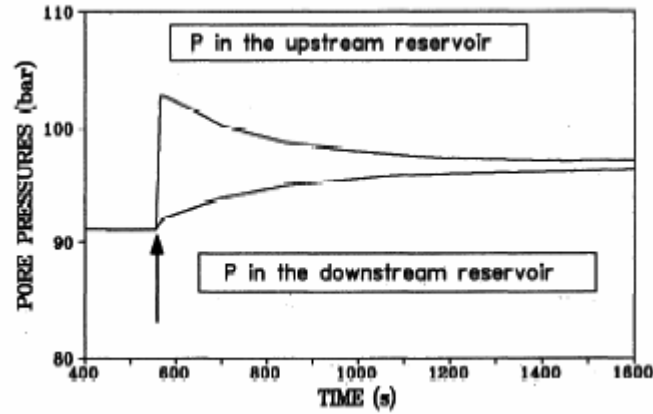


Fig. 5a. : Pulse decay as a function of time measured at maximum permeability. The arrow indicates the timing of the applied pressure pulse.

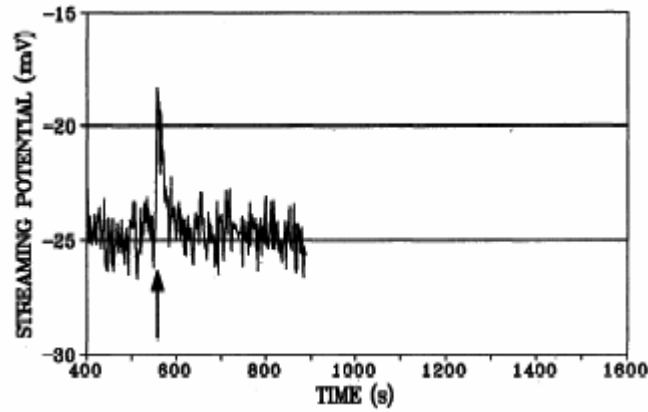


Fig. 5b. : Streaming potential as a function of time. The streaming potential only occurred in Zone III of strain (Fig.1) when the pore pressure pulse was just applied. The permeability of the sample was  $3.8 \cdot 10^{-18} \text{ m}^2$ . The arrow indicates the timing of the applied pressure pulse.

The streaming potential was not measurable when the sample had a low permeability (zone I), but clearly occurred when the permeability increased (zone III). As shown in Figures 5a and 5b, electrical noise was recorded before the pore pressure pulse  $\Delta P_0$  was applied and during the diffusion of the pore pressure. The streaming potential occurred just when the pore pressure pulse was applied. For this example,  $\Delta P_0$  is 11.7 bar, the streaming potential was 6 mV (-25 mV to -19 mV) while the noise was 2.5 mV. The same phenomenon was observed in the next state of deformation studied, when permeability was  $3.2 \cdot 10^{-19} \text{ m}^2$  (the last point in Figure 1). The streaming potential,



produced by fluid percolation when a fluid is made to flow through a porous medium, is theoretically proportional to the driving pore pressure [Overbeek, 1952; Nourbehecht, 1963; Dukhin and Derjaguin, 1974; Morgan et al., 1989].  $C = \Delta V / \Delta P = -(\epsilon \zeta) / (\eta \sigma)$  is called the electrokinetic coupling coefficient and depends on the fluid conductivity  $\sigma$ , the fluid viscosity  $\eta$ , the zeta potential  $\zeta$  (potential at the rock/fluid interface), and the dielectric constant of fluid  $\epsilon$ .

When the permeability of a sample is less than  $10^{-17} \text{ m}^2$ , the transient flow is described by a pressure diffusion law [Brace, 1968], and the volume flowing in the sample is the storage of fluid, due to the compressibilities of the fluid and of the solid. The evolution of the streaming potential with time is

$$\Delta V(t) = \frac{1}{\sigma} \cdot \int_{x_1}^{x_2} i_{\text{conv}}(t) dx, \text{ where } i_{\text{conv}}(t) = \frac{C \sigma}{\partial x} \frac{\partial P(t)}{\partial x} \quad (2)$$

and  $x_2 - x_1$  is the length of the sample. If we assume that  $C$  is constant,  $\Delta V(t) = C \Delta P(t)$ , the pressure gradient being constant along the length of the sample although it varies with time. The maximum streaming potential occurs when the pore pressure pulse  $\Delta P$  is maximum. The streaming potential strongly decreased and was no longer measurable when  $\Delta P$  fell below a critical value of 8 bar in our example.  $\Delta V$  and  $\Delta P$  showed two different time constants, 40 s and 165 s respectively, defined as the time when the signal decreased to half of its initial value. When  $\Delta P_0$  was applied, the Darcy's speed was 3.5 m/an, whereas it was 2.4 m/an when  $\Delta P$  fell to this critical value. It seems that the volume flowing in the sample was not sufficient to produce a measurable streaming potential, as when a decrease in the permeability of a sample of sandstone induces a decrease in the electrokinetic coupling coefficient [Pozzi and Jouniaux, 1993].

### Discussion and conclusion

The permeability of the indurated claystone increased almost by two orders of magnitude (from  $5 \cdot 10^{-20} \text{ m}^2$  to  $3.8 \cdot 10^{-18} \text{ m}^2$ ) when exposed to a deviatoric stress, even at small strain (0.015). We observed an unstable zone (zone II) where the permeability was unstable with time, at the same strain and without noticeable stress relaxation. When the sample was further deformed, the permeability remained high. Permeability showed only a slight variation with

effective pressure at low axial strain and became very sensitive to the effective pressure at greater axial strain (from  $3.2 \cdot 10^{-18} \text{ m}^2$  to  $1.7 \cdot 10^{-19} \text{ m}^2$ ) in the range of effective pressure from 2.3 to 10.8 MPa. The streaming potential became measurable in Zone III. At a permeability greater than  $3 \cdot 10^{-18} \text{ m}^2$ , a 6 mV streaming potential was produced in response to a pressure pulse of 1.17 MPa.

Although performed on only one sample, progressive shear deformation of an initially underformed sample from below the décollement is intended to approximate what happens to sequences of similar lithology that are naturally deformed above the décollement. Based on the geometry of the brittle structures in hole 808C, Lallemand et al. [1993] proposed that the 200m thick deformed claystone from above the décollement was subjected to high pore fluid pressure. Our experiments suggest that a shear strain under low effective pressure may be the cause of increased vertical permeability of these hemipelagic sequences. This increase of permeability may be detected by measuring the streaming potential. The streaming potential will be enhanced in cases of fresh water circulation relative to sea water circulation, because of the greater resistivity of fresh water. Changes of flow rates of fluids expelled from an accretionary wedge could be detected by monitoring changes of electrokinetic potential, as proposed by Boulègue et al. [1985], and related to the state of stress and the seismic hazard.

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Jouniaux et al. : Permeability and Streaming Potential of a Nankai Claystone under Stress